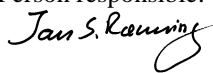


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Helicopter-borne magnetic, electromagnetic  
and radiometric geophysical survey at  
Andøya, Nordland County.



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<b>Summary:</b> <p>NGU conducted an airborne geophysical survey in Andøya area in August – September 2012. This report describes and documents the acquisition, processing and visualization of recorded datasets. The geophysical survey results reported herein are 2614 line km.</p> <p>The Geotech Ltd. Hummingbird frequency domain system supplemented by optically pumped Caesium magnetometer and 1024 channels RSX-5 spectrometer was used for data acquisition. The survey was flown with 200 m line spacing, line direction of 90° W-E with the average speed 90 km/h. The average terrain clearance of the bird was 56 m.</p> <p>Collected data were processed by AR Geoconsult ltd. using Geosoft Oasis Montaj software. Raw total magnetic field data were corrected for diurnal variation and levelled using standard micro levelling algorithm. EM data were filtered and levelled using both automated and manual levelling procedure. Apparent resistivity was calculated from in-phase and quadrature data for each of the five frequencies separately using a homogeneous half space model. Apparent resistivity dataset was levelled and filtered. Radiometric data were processed using standard procedures recommended by International Atomic Energy Association.</p> <p>All data were gridded with the cell size of 50 m and presented as a maps at the scale of 1:50 000.</p>			
<b>Keywords:</b> Geophysics	Airborne	Magnetic	
Electromagnetic	Gamma spectrometry	Radiometric	
		Technical report	

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## 1. INTRODUCTION

In 2011 the Norwegian government initiated a new program for mapping of mineral resources in Northern Norway (MINN). The goal of this program is to enhance the geological information that is relevant to an assessment of the mineral potential of the three northernmost counties. The airborne geophysical surveys - helicopter borne and fixed wing- are important integral part of MINN program. The helicopterborne survey results reported herein amount to 2614 line km (523 km<sup>2</sup>) over the island Andøya, as shown in **Feil! Fant ikke referanseikilden..**

The objective of the airborne geophysical survey was to obtain a dense high-resolution aero-magnetic, electromagnetic and radiometric data over the survey area. This data is required for the enhancement of a general understanding of the regional geology of the area. In this regard, the data can also be used to map contacts and structural features within the property. It also allow to better define the potential of known zones of mineralization, their geological settings and identify new areas of interest.

The survey incorporated the use of a Hummingbird™ five-frequency electromagnetic system supplemented by a high-sensitivity Cesium magnetometer, gamma ray spectrometer, barometric altimeter, and radar altimeter. A GPS navigation computer system with flight path indicators ensured accurate positioning of the geophysical data with respect to the World Geodetic System 1984 geodetic datum (WGS-84).



Figure 1: Andøya survey. Location map.

## **2. SURVEY SPECIFICATIONS**

### **2.1 Airborne Survey Parameters**

NGU used a Hummingbird™ electromagnetic and magnetic helicopter survey system designed to obtain low level, slow speed, detailed airborne magnetic and electromagnetic data (Geotech 1997). In addition, a 1024 channel Gamma Spectrometer installed under the belly of the helicopter registered natural gamma ray radiation simultaneously with the acquisition of magnetic/EM data.

The airborne survey began on August 28 and ended on September 9 2012. A Eurocopter AS350-B2 helicopter was used to tow the bird. The survey lines were spaced 200 m apart. Lines were oriented at 90° W-E. The magnetic and electromagnetic sensors are housed in a single 7.5 m long bird, which was maintained at an average of 56 m above the topographic surface.

Rugged terrain and abrupt changes in topography affect the aircraft pilot's ability to 'drape' the terrain; therefore there are positive and negative variations in sensor height with respect to the estimated range, which is higher than the standard height of 30 m. The ground speed of the aircraft varied from 30 – 120 km/h depending on topography, wind direction and its magnitude. On average the ground speed is estimated to be 90 km/h. Magnetic data were recorded 5 times a second giving a average point spacing of about 5 meters. The electromagnetic system was recorded at 0.1 second intervals resulting in an average points spacing less than 3 meters. Spectrometry data were accumulated every 1 second, over a distance of 25 meters in average. The above parameters were designed to allow for sufficient detail in the data to detect subtle anomalies that may represent mineralization and/or rocks of different lithological and petrophysical composition.

A base magnetometer to monitor diurnal variations in the magnetic field was located at Andenes Airport in the northern end of the survey area. Scintrex EnviMAG station magnetometer data were recorded once every 3 seconds. The CPU clock of the base magnetometer and the helicopter magnetometer were both synchronized to GMT (Greenwich MeanTime) through the built-in GPS receiver to allow correction of diurnals.

Navigation system uses GPS satellite tracking systems to provide real-time WGS-84 coordinate locations for every second. The accuracy achieved with no differential corrections is reported to less than  $\pm 5$  m in the horizontal directions.

### **2.2 Airborne Survey Instrumentation**

Instrument specification is given in table 1. Frequencies and coil configuration for the Hummingbird EM system is given in table 2.

**Table 1. Instrument Specifications**

<b>Instrument</b>	<b>Producer/Model</b>	<b>Accuracy</b>	<b>Sampling frequency/interval</b>
Magnetometer	Scintrex Cs-2	0,002 nT	5 Hz
Base magnetometer	Scintrex EnviMAG	0.1 nT	3 sec
Electromagnetic	Geotech Hummingbird	1 – 2 ppm	10 Hz
Gamma spectrometer	Radiation Solutions RSX-5	1024 channels, 16 liters down, 4 liters up	1 Hz 1 sec accumulation
Radar altimeter	Bendix/King KRA 405B	± 3 % 0 – 500 feet ± 5 % 500 – 2500 feet	1 Hz
Pressure/temperature	Honeywell PPT	± 0,03 % FS	1 Hz
Navigation	Topcon GPS-receiver	± 5 meter	1 Hz
Acquisition system	PC based in house software		

**Table 2. Hummingbird electromagnetic system, frequency and coil configurations**

<b>Coils:</b>	<b>Frequency</b>	<b>Orientation</b>	<b>Separation</b>
A	7700 Hz	Coaxial	6.20 m
B	6600 Hz	Coplanar	6.20 m
C	980 Hz	Coaxial	6.025 m
D	880 Hz	Coplanar	6.025 m

## 2.3 Airborne Survey Logistics Summary

Traverse (survey) line spacing: 200 metres

Traverse line direction: 90° W-E

Nominal aircraft ground speed: 30 - 120 km/h

Average sensor terrain clearance: 56 metres

Sampling rates:

- 0.2 seconds - magnetometer
- 0.1 seconds - electromagnetics
- 1.0 second - spectrometer, GPS, altimeter





**Figure 2: Hummingbird system in the air**

### 3. DATA PROCESSING AND PRESENTATION

All data were processed by Alexei Rodionov (AR Geoconsulting Ltd., Canada) in Calgary. The ASCII data files were loaded into three separate Oasis Montaj databases. All three datasets were processed consequently according to processing flow charts shown in Appendix A1, A2 and A3.

#### 3.1 Total Field Magnetic Data

All magnetic data (in line and base station) were within the standard NGU specifications during the entire survey (Rønning 2013). At the first stage the raw magnetic data were visually inspected and spikes were removed manually. Non-linear filter was also applied to airborne raw data to eliminate short-period spikes. Typically, several corrections have to be applied to magnetic data before gridding - heading correction, lag correction and diurnal correction.

##### Diurnal Corrections

The temporal fluctuations in the magnetic field of the earth affect the total magnetic field readings recorded during the airborne survey. This is commonly referred to as the magnetic diurnal variation. These fluctuations can be effectively removed from the airborne magnetic dataset by using a stationary reference magnetometer that records the magnetic field of the earth simultaneously with the airborne sensor at given short time interval. The data from base station were imported in database using the standard Oasis magbase.gx module. Diurnal variation channel was inspected for spikes and spikes were removed manually if necessary.

The base magnetometer (Scintrex EnviMAG proton magnetometer) was located at the Andenes airport, in the northern end of the survey area. The average total field value for this point was 53103 nT. The recorded data are merged with the airborne data and the diurnal correction is applied according to equation (1).

$$\mathbf{B}_{Tc} = \mathbf{B}_T + (\bar{\mathbf{B}}_B - \mathbf{B}_B), \quad (1)$$

where:

$\mathbf{B}_{Tc}$  = Corrected airborne total field readings

$\mathbf{B}_T$  = Airborne total field readings

$\bar{\mathbf{B}}_B$  = Average datum base level

$\mathbf{B}_B$  = Base station readings

##### Corrections for Lag and heading

Neither a lag nor cloverleaf tests were performed before the survey. According to previous reports the lag between logged magnetic data and the corresponding navigational data was 1-2 fids. Translated to a distance it would be no more than 10 m - the value comparable with the precision of GPS. A heading error for a towed system is usually either very small or non-existent. So no lag and heading corrections were applied.

##### Magnetic data processing, gridding and presentation

The total field magnetic anomaly data ( $\mathbf{B}_{TA}$ ) were calculated from the diurnal corrected data

( $\mathbf{B}_{Tc}$ ) after subtracting the IGRF for the surveyed area calculated for the data period (eq.2)

$$\mathbf{B}_{TA} = \mathbf{B}_{Tc} - IGRF \quad (2)$$

The total field anomaly data were gridded using a minimum curvature method with a grid cell size of 50 meters. This cell size is equal to one quarter of the 200 m average line spacing. In order to remove small line-to-line levelling errors that were detected on the gridded magnetic anomaly data, the Geosoft Micro-levelling technique was applied on the flight line based magnetic database. Then, the micro-levelled channel was gridded using again a minimum curvature method with 50 m grid cell size. Finally, 3x3 convolution filter was applied to smooth the grid.

The processing steps of magnetic data presented so far, were performed on point basis. The following steps are performed on grid basis. **Vertical Gradient** along with the **Tilt Derivative** of the total magnetic anomaly was calculated from the micro-levelled total magnetic anomaly grid. The Tilt derivative (TD) was calculated according to the equation (3)

$$TD = \tan^{-1} \left( \frac{VG}{HG} \right) \quad (3)$$

The results are presented in coloured shaded relief maps:

- A. Total field magnetic anomaly
- B. Vertical gradient of total magnetic anomaly
- C. Tilt angle (or Tilt Derivative) of the total magnetic anomaly

These maps are representative of the distribution of magnetization over the surveyed areas. The list of the produced maps is shown in Feil! Fant ikke referansekilden..

### 3.2 Electromagnetic Data

The Geotech Hummingbird system records both an in-phase and a quadrature value for each of the five coil sets of the electromagnetic system. Instrumental noise and drift should be removed before computation of an apparent resistivity.

#### Instrumental noise

In-phase and quadrature data were filtered with 3 fids non-linear filter to eliminate spheric spikes which were represented as irregular spikes of large amplitude in records. Simultaneously, the 30 fids low-pass filter was also applied to suppress high frequency components of instrumental and cultural noise. In general, the cultural noise in the survey area was low and almost completely was suppressed by filtering.

#### Instrument Drift

In order to remove the effects of instrument drift caused by gradual temperature variations in the transmitting and receiving circuits, background responses are recorded during each flight. To obtain a background level the bird is raised to an altitude of at least 1000 ft above the topographic surface so that no electromagnetic responses from the ground are present in the recorded traces. The EM traces observed at this altitude correspond to a background (zero) level of the system. If these background levels are recorded at 20-30 minute intervals, then the drift of the system (assumed to be linear) can be removed from the data by resetting these

points to the initial zero level of the system. The drift must be removed on a flight-by-flight basis, before any further processing is carried out. Geosoft HEM module was used for applying drift correction. Residual instrumental drift, usually small, but non-linear, was manually removed on line-to-line basis.

### **Apparent resistivity calculation and presentation**

When levelling of the EM data was complete, apparent resistivity was calculated from in-phase and quadrature EM components using a half space homogeneous model of the Earth (Geosoft HEM module) for all five frequencies separately. Threshold of 2 ppm was set for inversion of 34 kHz and 6.6 kHz data, 1 ppm for all other frequencies.

Secondary electromagnetic field decays rapidly with the distance (height of the sensors) – as  $z^{-2} - z^{-5}$  depending on the shape of the conductors and, at certain height, signals from the ground sources become comparable with instrumental noise. Levelling errors or precision of levelling can lead sometimes to appearance of artificial resistivity anomalies when data were collected at high instrumental altitude. Application of threshold allows excluding such data from an apparent resistivity calculation, though not completely. It's particularly noticeable in low frequencies datasets. Resistivity data were visually inspected; artificial anomalies associated with high altitude measurements were manually removed.

Data, recorded at the height above 100 m were considered as non-reliable and removed from presentation. Remaining resistivity data were gridded with a cell size 50 m and 3x3 convolution filter was applied to smooth resistivity grids.

### **3.3 Radiometric data**

Airborne gamma-ray spectrometry measures the abundance of Potassium (K), Thorium (eTh), and Uranium (eU) in rocks and weathered materials by detecting gamma-rays emitted due to the natural radioelement decay of these elements. The data analysis method is based on the IAEA recommended method for U, Th and K (International Atomic Energy Agency, 1991; 2003). A short description of the individual processing steps of that methodology as adopted by NGU is given bellow. All radiometric data from Andøya survey were within standard NGU specifications (Rønning 2013).

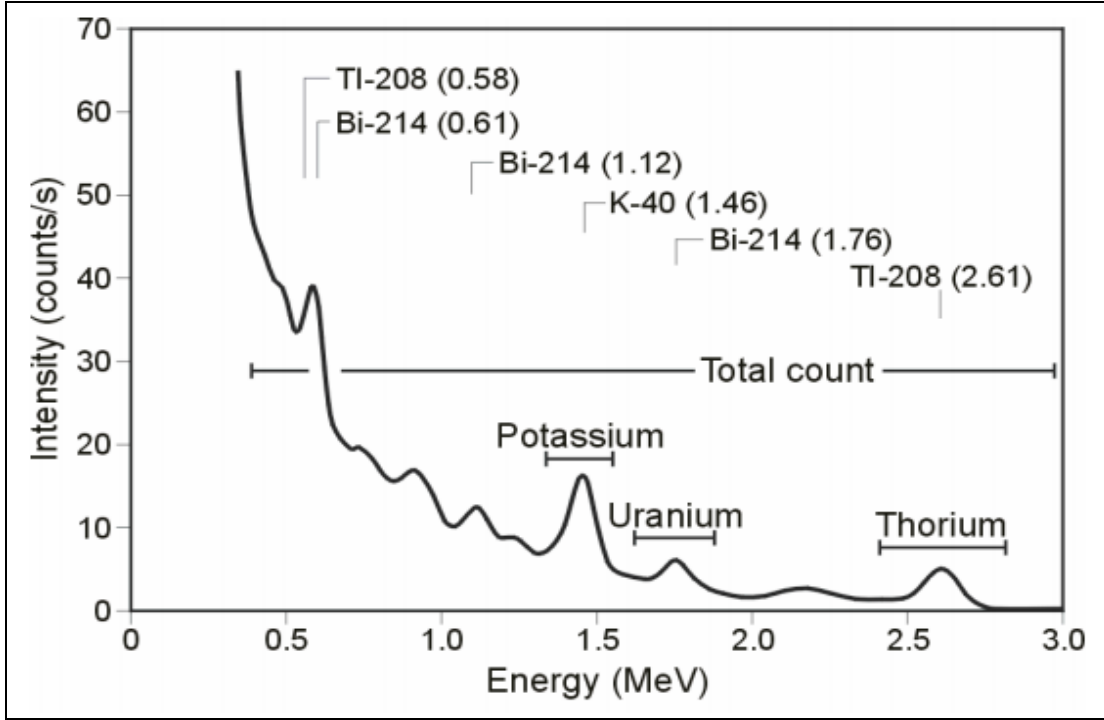
#### **Energy windows**

The Gamma-ray spectra were initially reduced into standard energy windows corresponding to the individual radio-nuclides K, U and Th. **Figure 3** shows an example of a Gamma-ray spectrum and the corresponding energy windows and radioisotopes (with peak energy in MeV) responsible for the radiation.

The RSX-5 is a 1024 channel system with four downward and one upward looking detectors and the actual Gamma-ray spectrum is divided into 1024 channels. The first channel is reserved for the “Live Time” and the last for the Cosmic rays. **Table 3** shows the channels that were used for the reduction of the spectrum.

**Table 3: Specified channel windows for the 1024 RSX-5 systems used in this survey**

<b>Gamma-ray spectrum</b>	<b>Cosmic</b>	<b>Total count</b>	<b>K</b>	<b>U</b>	<b>Th</b>
<b>Down</b>	<b>1022</b>	<b>134-934</b>	<b>454-521</b>	<b>551-617</b>	<b>801-934</b>
<b>Up</b>	<b>1022</b>			<b>551-617</b>	
<b>Energy windows (MeV)</b>	<b>&gt;3.07</b>	<b>0.41-2.81</b>	<b>1.37-1.57</b>	<b>1.66-1.86</b>	<b>2.41-2.81</b>



**Figure 3: An example of Gamma-ray spectrum showing the position of the K, Th, U and Total count windows (Peak energy in brackets).**

### Live Time correction

The data were corrected for live time. “Live time” is an expression of the relative period of time the instrument was able to register new pulses per sample interval. On the other hand “dead time” is an expression of the relative period of time the system was unable to register new pulses per sample interval. The relation between “dead” and “live time” is given by the equation (4)

$$\text{“Live time”} = \text{“Real time”} - \text{“Dead time”} \quad (4)$$

where the “real time” or “acquisition time” is the elapsed time over which the spectrum is accumulated (1 second).

The live time correction is applied to the total count, Potassium, Uranium, Thorium, upward Uranium and cosmic channels. The formula used to apply the correction is as follows:

$$C_{LT} = C_{RAW} \cdot \frac{1000000}{\text{Live Time}} \quad (5)$$

where  $C_{LT}$  is the live time corrected channel in counts per second,  $C_{RAW}$  is the raw channel data in counts per second and Live Time is in microseconds.

To improve counting statistics, 5 fid low pass filter was applied to Uranium and 3 fid low pass filter was applied to Thorium live time corrected data.

### Cosmic and aircraft correction

Background radiation resulting from cosmic rays and aircraft contamination was removed from the total count, Potassium, Uranium, Thorium, upward Uranium channels using the following formula:

$$C_{CA} = C_{LT} - (a_c + b_c \cdot C_{Cos}) \quad (6)$$

where  $C_{CA}$  is the cosmic and aircraft corrected channel,  $C_{LT}$  is the live time corrected channel  $a_c$  is the aircraft background for this channel,  $b_c$  is the cosmic stripping coefficient for this channel and  $C_{Cos}$  is the low pass filtered cosmic channel.

### Radon correction

The upward detector method, as discussed in IAEA (1991), was applied to remove the effects of the atmospheric radon in the air below and around the helicopter. Usages of over-water measurements where there is no contribution from the ground, enabled the calculation of the coefficients ( $a_c$  and  $b_c$ ) of the linear equations that relate the cosmic corrected counts per second of Uranium channel with total count, Potassium, Thorium and Uranium upward channels over water. Data over-land was used in conjunction with data over-water to calculate the  $a_1$  and  $a_2$  coefficients used in equation (7) for the determination of the Radon component in the downward uranium window:

$$Radon_U = \frac{Uup_{CA} - a_1 \cdot U_{CA} - a_2 \cdot Th_{CA} + a_2 \cdot b_{Th} - b_U}{a_U - a_1 - a_2 \cdot a_{Th}} \quad (7)$$

where  $Radon_u$  is the radon component in the downward uranium window,  $Uup_{CA}$  is the filtered upward uranium,  $U_{CA}$  is the filtered Uranium,  $Th_{CA}$  is the filtered Thorium,  $a_1$ ,  $a_2$ ,  $a_U$  and  $a_{Th}$  are proportional factors and  $b_U$  and  $b_{Th}$  are constants determined experimentally.

The effects of Radon in the downward Uranium are removed by simply subtracting  $Radon_U$  from  $U_{CA}$ . The effects of radon in the other channels are removed using the following formula:

$$C_{RC} = C_{CA} - (a_c \cdot Radon_U + b_c) \quad (8)$$

where  $C_{RC}$  is the Radon corrected channel,  $C_{CA}$  is the cosmic and aircraft corrected channel,  $Radon_U$  is the Radon component in the downward uranium window,  $a_c$  is the proportionality factor and  $b_c$  is the constant determined experimentally for this channel from over-water data.

### Compton Stripping

Potassium, Uranium and Thorium Radon corrected channels, are subjected to spectral overlap correction. Compton scattered gamma rays in the radio-nuclides energy windows were corrected by window stripping using Compton stripping coefficients determined from measurements on calibrations pads at the Geological Survey of Norway in Trondheim (Grasty et al. 1991, for values see Appendix A3).

The stripping corrections are given by the following formulas:

$$A_1 = 1 - (g \cdot \gamma) - (a \cdot \alpha) + (a \cdot g \cdot \beta) - (b \cdot \beta) + (b \cdot \alpha \cdot \gamma) \quad (9)$$

$$U_{ST} = \frac{Th_{RC} \cdot ((g \cdot \beta) - \alpha) + U_{RC} \cdot (1 - b \cdot \beta) + K_{RC} \cdot ((b \cdot \alpha) - g)}{A_1} \quad (10)$$

$$Th_{ST} = \frac{Th_{RC} \cdot (1 - (g \cdot \gamma)) + U_{RC} \cdot (b \cdot \gamma - a) + K_{RC} \cdot ((a \cdot g) - b)}{A_1} \quad (11)$$

$$K_{ST} = \frac{Th_{RC} \cdot ((\alpha \cdot \gamma) - \beta) + U_{RC} \cdot ((a \cdot \beta) - \gamma) + K_{RC} \cdot (1 - (a \cdot \alpha))}{A_1} \quad (12)$$

where  $U_{RC}$ ,  $Th_{RC}$ ,  $K_{RC}$  are the radon corrected Uranium, Thorium and Potassium and  $a$ ,  $b$ ,  $g$ ,  $\alpha$ ,  $\beta$ ,  $\gamma$  are Compton stripping coefficients.

### Reduction to Standard Temperature and Pressure

The radar altimeter data were converted to effective height ( $H_{STP}$ ) using the acquired temperature and pressure data, according to the expression:

$$H_{STP} = H \cdot \frac{273.15}{T + 273.15} \cdot \frac{P}{1013.25} \quad (13)$$

where  $H$  is the smoothed observed radar altitude in meters,  $T$  is the measured air temperature in degrees Celsius and  $P$  is the measured barometric pressure in millibars.

### Height correction

Variations caused by changes in the aircraft altitude relative to the ground was corrected to a nominal height of 60 m. Data recorded at the height above 150 m were considered as non-reliable and removed from processing. Total count, Uranium, Thorium and Potassium stripped channels were subjected to height correction according to the equation:

$$C_{60m} = C_{ST} \cdot e^{C_{ht}(60-H_{STP})} \quad (14)$$

where  $C_{ST}$  is the stripped corrected channel,  $C_{ht}$  is the height attenuation factor for that channel and  $H_{STP}$  is the effective height.

### Conversion to ground concentrations

Finally, corrected count rates were converted to effective ground element concentrations using calibration values derived from calibration pads at the Geological Survey of Norway in Trondheim (for values, see Appendix A3). The corrected data provide an estimate of the apparent surface concentrations of Potassium, Uranium and Thorium ( $K$ ,  $eU$  and  $eTh$ ). Potassium concentration is expressed as a percentage, equivalent Uranium and Thorium as parts per million (ppm). Uranium and Thorium are described as “equivalent” since their presence is inferred from gamma-ray radiation from daughter elements ( $^{214}Bi$  for Uranium,  $^{208}Tl$  for Thorium). The concentration of the elements is calculated according to the following expressions:

$$C_{CONC} = C_{60m} / C_{SENS\_60m} \quad (15)$$

where  $C_{60m}$  is the height corrected channel,  $C_{SENS\_60m}$  is experimentally determined sensitivity reduced to the nominal height (60m).

### **Spectrometry data gridding and presentation**

Gamma-rays from Potassium, Thorium and Uranium emanate from the uppermost 30 to 40 centimetres of soil and rocks in the crust (Minty 1997). Variations in the concentrations of these radioelements largely related to changes in the mineralogy and geochemistry of the Earth's surface.

The spectrometry data were stored in a database and the ground concentrations were calculated following the processing steps. A list of the parameters used in these steps is given in Appendix A3.

Then the data were split in lines and ground concentrations of the three main natural radioelements Potassium, Thorium and Uranium and total gamma-ray flux (total count) were gridded using a minimum curvature method with a grid cell size of 50 meters. In order to remove small line-to-line levelling errors appeared on those grids, the data were micro-levelled as in the case of the magnetic data, and re-gridded with the same grid cell size. Finally, a 3x3 convolution filter was applied to Uranium grid to smooth the microlevelled concentration grids.

Quality of the radiometric data was within standard NGU specifications (Rønning 2013). For further reading regarding standard processing of airborne radiometric data, we recommend the publications from Minty et al. (1997).



#### 4. PRODUCTS

Processed digital data from the survey are presented as:

1. Three Geosoft XYZ files: Andoya\_Mag.xyz, Andoya\_EM.xyz, Andoya\_Rad.xyz, available from NGU on request.
2. Georeferenced tiff files (Geotiff)
3. Coloured maps at the scale 1:50000 available from NGU on request.

**Table 4: Maps in scale 1:50000 available from NGU on request.**

Map #	Name
2012.056-01	Total magnetic field
2012.056-02	Total magnetic field. Vertical gradient
2012.056-03	Total magnetic field. Tilt derivative
2012.056-04	Apparent resistivity, Frequency 34000 Hz, coplanar coils
2012.056-05	Apparent resistivity, Frequency 6600 Hz, coplanar coils
2012.056-06	Apparent resistivity, Frequency 880 Hz, coplanar coils
2012.056-07	Apparent resistivity, Frequency 7000 Hz, coaxial coils
2012.056-08	Apparent resistivity, Frequency 980 Hz, coaxial coils
2012.056-09	Uranium ground concentration
2012.056-10	Thorium ground concentration
2012.056-11	Potassium ground concentration
2012.056-12	Ternary map
2012.056-13	Total count

Downscaled images of the maps are shown on figures 4 - 17

## 5. REFERENCES

Geotech 1997: Hummingbird Electromagnetic System. User manual. Geotech Ltd. October 1997

Grasty, R.L., Holman, P.B. & Blanchard 1991: Transportable Calibration pads for ground and airborne Gamma-ray Spectrometers. Geological Survey of Canada. Paper 90-23. 62 pp.

IAEA 1991: Airborne Gamma-Ray Spectrometry Surveying, Technical Report No 323, Vienna, Austria, 97 pp.

IAEA 2003: Guidelines for radioelement mapping using gamma ray spectrometry data. IAEA-TECDOC-1363, Vienna, Austria. 173 pp.

Minty, B.R.S. 1997: Fundamentals of airborne gamma-ray spectroscopy. . AGSO – Journal of Australian Geology & Geophysics. 17(2). 39-50.

Minty, B.R.S., Luyendyk, A.P.J. and Brodie, R.C. 1997: Calibration and data processing for gamma-ray spectrometry. AGSO – Journal of Australian Geology & Geophysics. 17(2). 51-62.

Naudy, H. and Dreyer, H. 1968: Non-linear filtering applied to aeromagnetic profiles. Geophysical Prospecting. 16(2). 171-178.

Rønning, J.S. 2013: NGUs helikoptermålinger. Plan for sikring og kontroll av datakvalitet. NGU Intern rapport 2013.001, (38 sider).

## 6. Appendix A1: Flow chart of magnetic processing

Meaning of parameters is described in the referenced literature.

Processing flow:

- Quality control.
- Visual inspection of airborne data and manual spike removal
- Conversion of ASCII data file from magbase station to Geosoft \*.bas files
- Import magbase data to Geosoft database
- Inspection of magbase data and removal of spikes
- Correction of data for diurnal variation
- Conversion of WGS-84 geographic coordinates to UTM 33N coordinates
- Splitting flight data by lines
- IGRF calculation and subtraction of IGRF from observed total field.
- Gridding
- Microlevelling

## 7. Appendix A2: Flow chart of EM processing

Meaning of parameters is described in the referenced literature.

Processing flow:

- Filtering of in-phase and quadrature channels with non-linear and low pass filters
- Automated leveling
- Quality control
- Visual inspection of data.
- Conversion of WGS-84 geographic coordinates to UTM 33N coordinates
- Splitting flight data by lines
- Manual removal of remaining part of instrumental drift
- Calculation of an apparent resistivity for each frequency
- Manual removal of artificial resistivity anomalies
- Microlevelling of apparent resistivity.
- Gridding
- Convolution filter.

## 8. Appendix A3: Flow chart of radiometry processing

Underlined processing stages are not only applied to the K, U and Th window, but also to the total count.

Meaning of parameters is described in the referenced literature.

Processing flow:

- Quality control
- Conversion of WGS-84 geographic coordinates to UTM 33N coordinates
- Splitting flight data to lines
- Calculation U,Th,K,TC windows
- Livetime correction
- Airborne and cosmic correction (IAEA, 2003)

Used parameters: (determined by high altitude calibration flights near Seljord in June 2012)

Aircraft background counts:

K window	7
U window	2
Th window	0
Uup window	0
Total counts	44

Cosmic background counts (normalized to unit counts in the cosmic window):

K window	0.0701
U window	0.0463
Uup window	0.0505
Th window	0.0664
Total counts	1.1228

- Radon correction using upward detector method (IAEA, 2003)  
Used parameters (determined from survey data over water and land):

$a_u$ : 0.1461	$b_u$ : 0.931
$a_K$ : 4.8199	$b_K$ : 0.1747
$a_T$ : 0.4818	$b_T$ : 0.4843
$a_{TC}$ : 41.969	$b_{TC}$ : 0.2657
$a_1$ : 0.0891	$a_2$ : -0.0117
- Stripping correction (IAEA, 2003)  
Used parameters (determined from measurements on calibrations pads at the NGU and Borlänge airport):

a	0.04840;
b	-0.00121;
g	-0.00074;
alpha	0.2999
beta	0.4755
gamma	0.8314
- Height correction to a height of 60 m  
Used parameters (determined by height calibration flight at near Seljord in June 2012):  
Attenuation factors in 1/m:

K:	-0.0072
U:	-0.0058
Th:	-0.0058
Total counts:	-0.0056
- Converting counts at 60 m heights to element concentration on the ground  
Used parameters (determined from measurements on calibrations pads at the NGU and Borlänge airport):  
Counts per elements concentrations:

K:	0.00757 %/counts
U:	0.087834 ppm/counts
Th:	0.154092 ppm/counts
- Microlevelling using Geosoft menu  
Used parameters for microlevelling:

De-corrugation cutoff wavelength:	800 m
Cell size for gridding:	50 m
Naudy (1968) Filter length:	800 m



Figure 4: Andøya survey. Flight path.



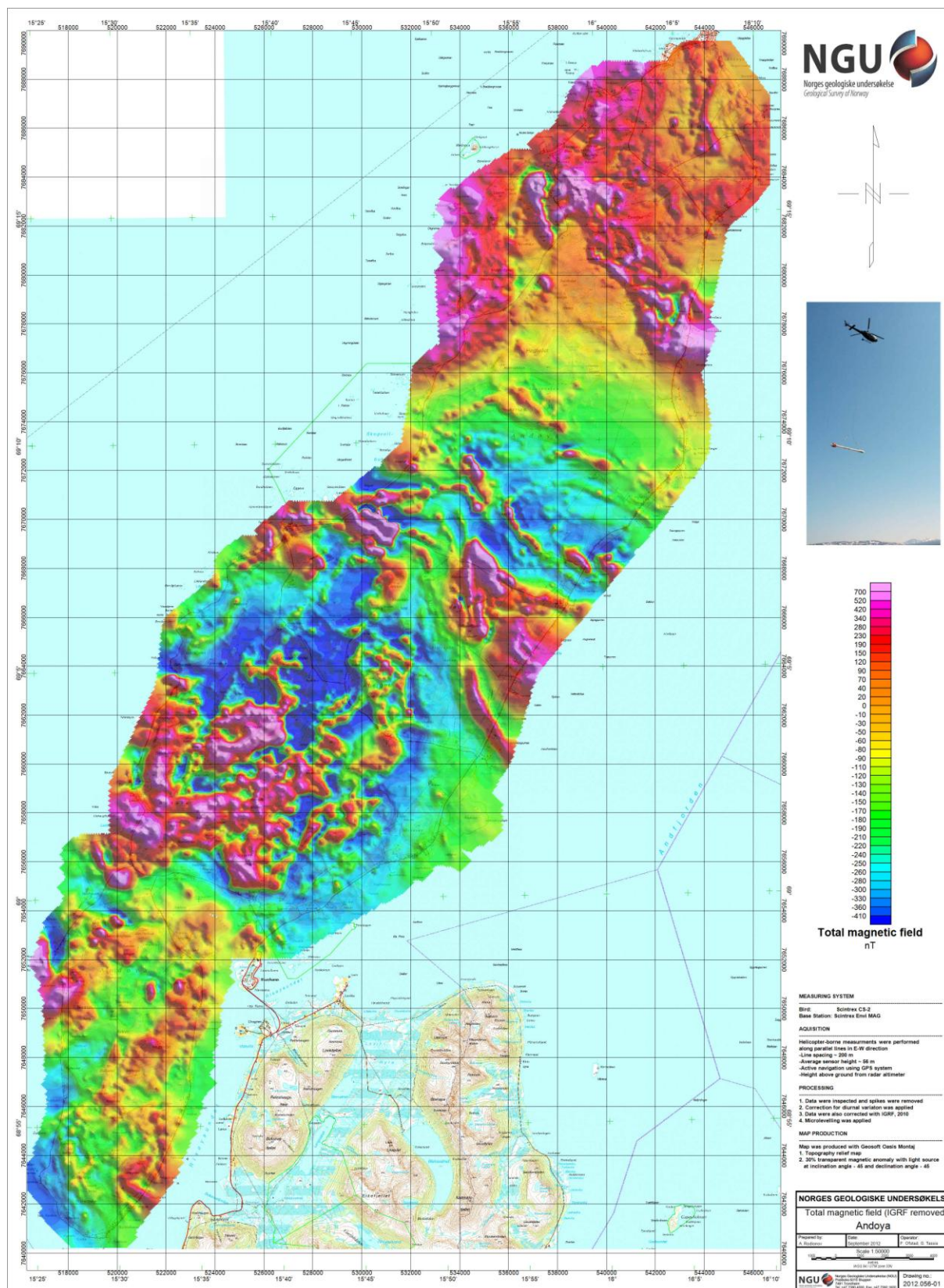


Figure 5: Total magnetic field



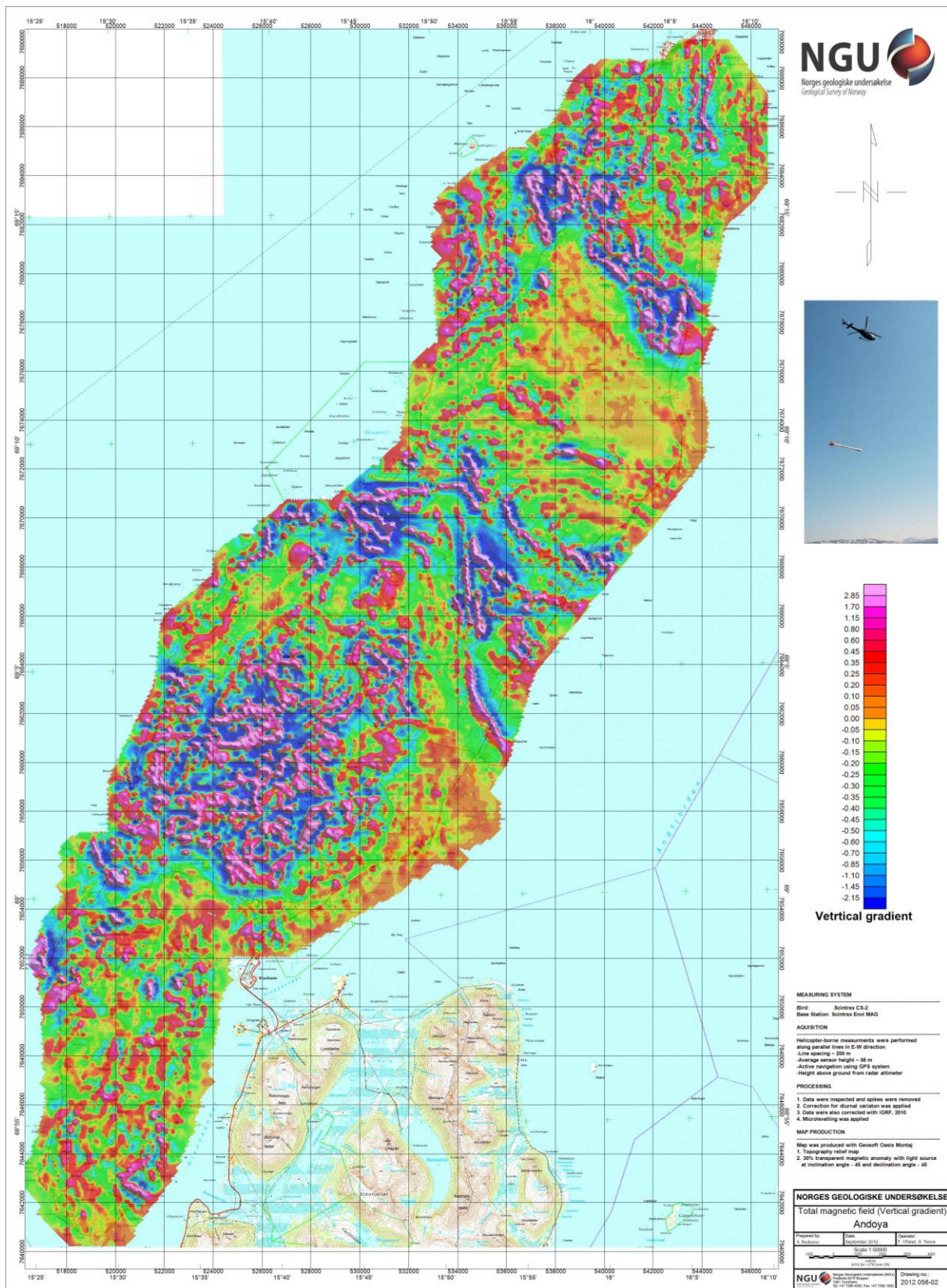


Figure 6: Total magnetic field. Vertical gradient.



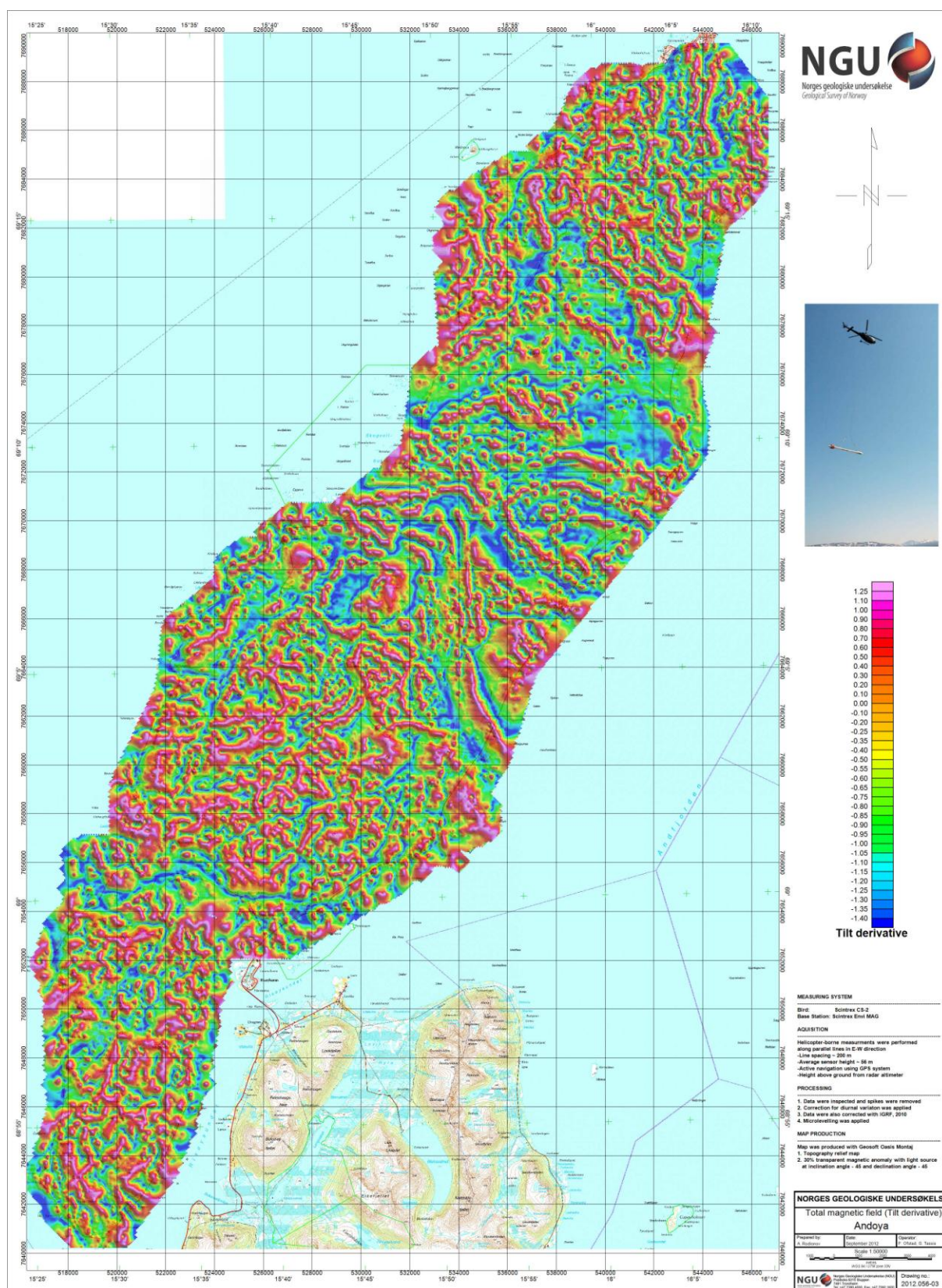


Figure 7: Total magnetic field. Tilt derivative.



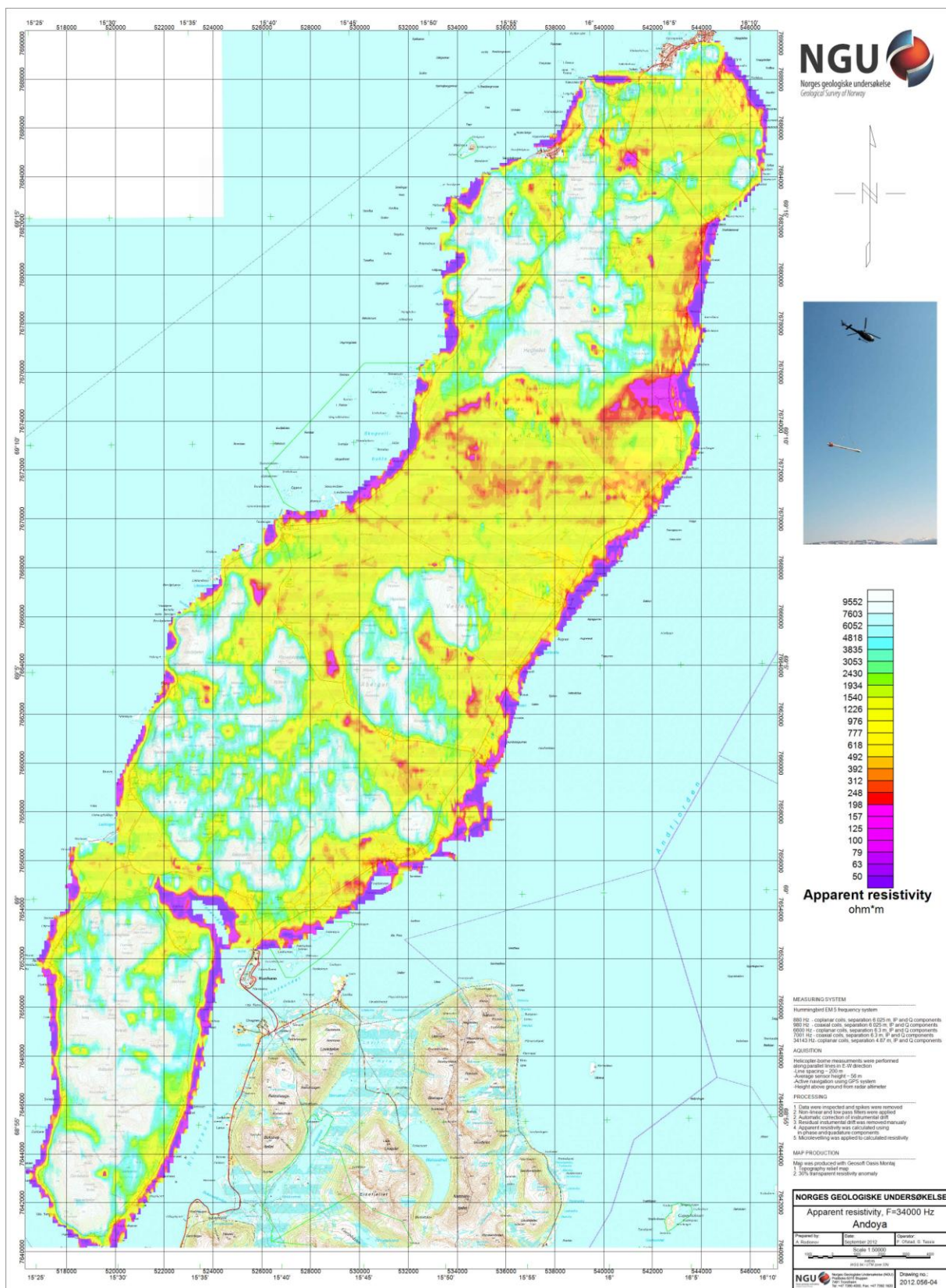


Figure 8: Apparent resistivity. Frequency 34000 Hz, Coplanar coils

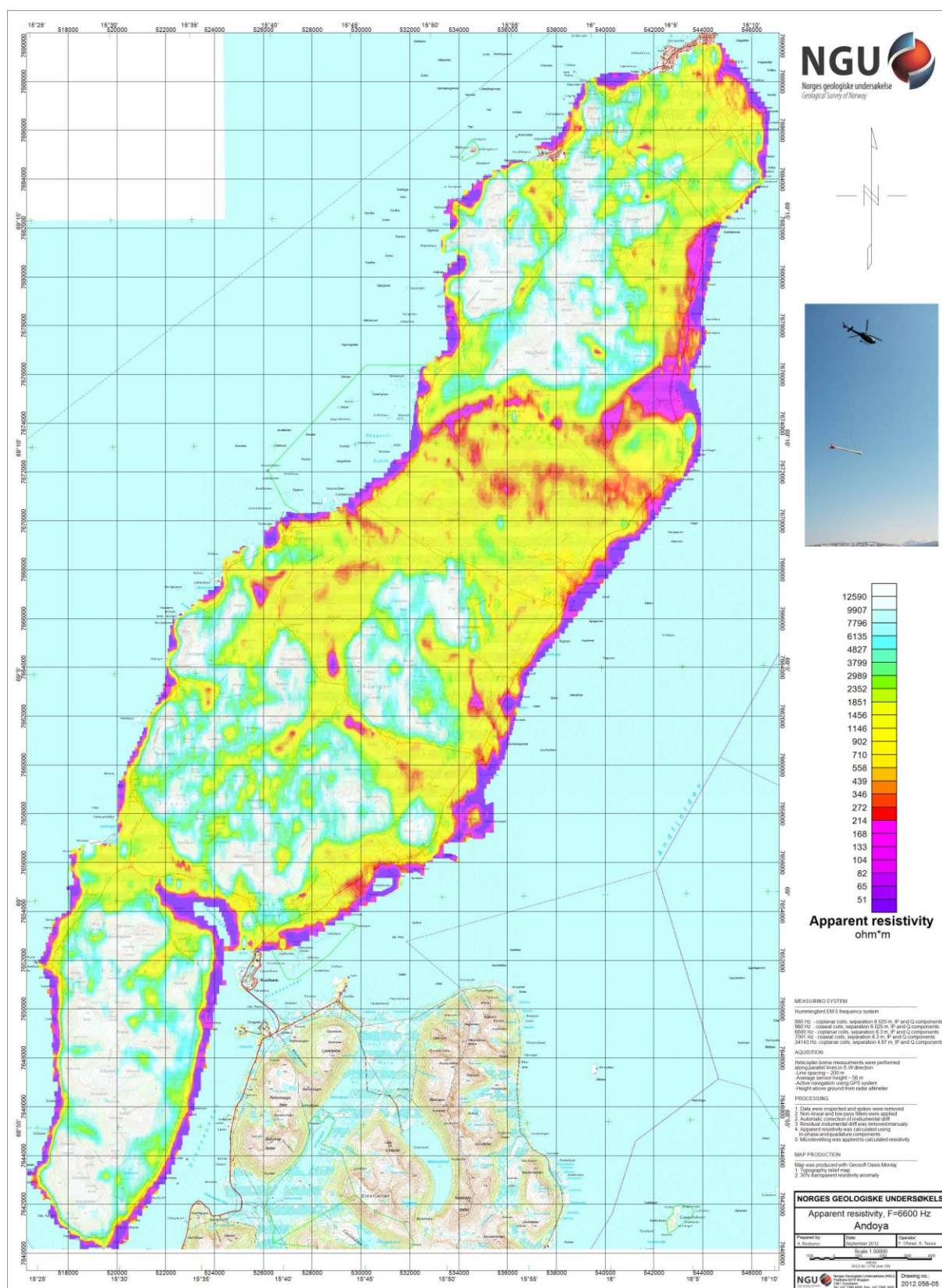


Figure 9: Apparent resistivity. Frequency 6600 Hz, Coplanar coils



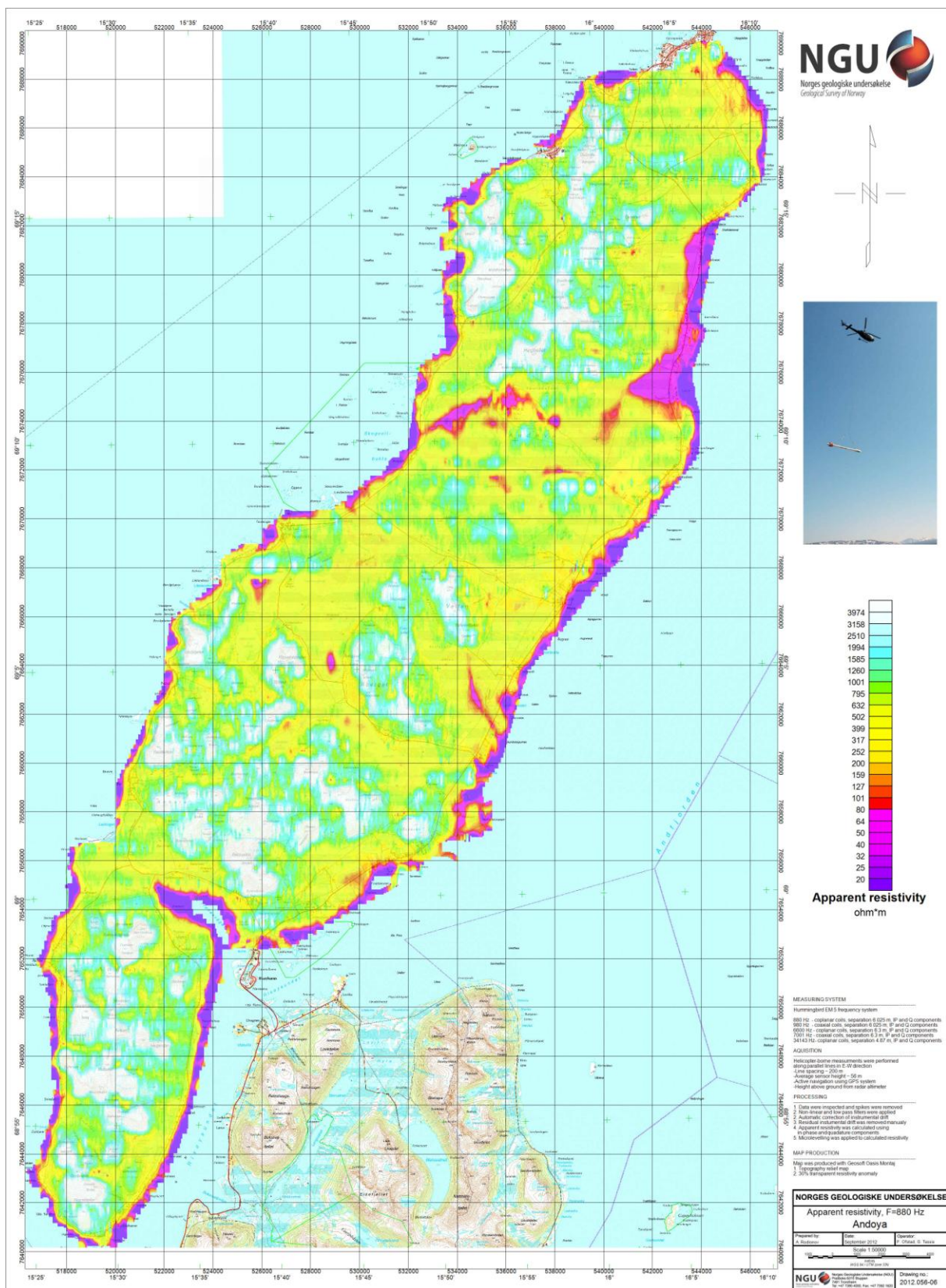


Figure 10: Apparent resistivity. Frequency 880 Hz, Coplanar coils

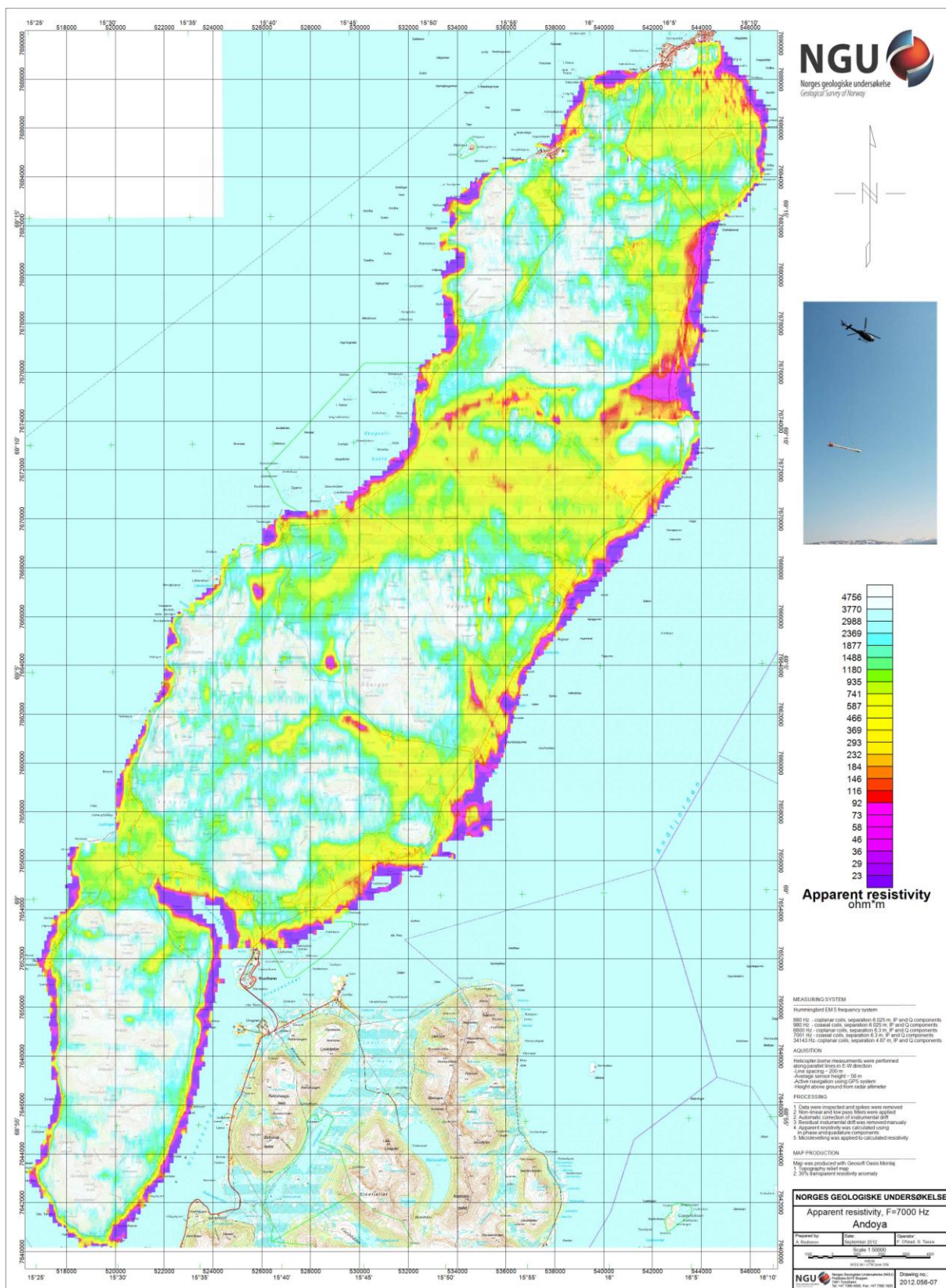


Figure 11: Apparent resistivity. Frequency 7000 Hz, Coaxial coils



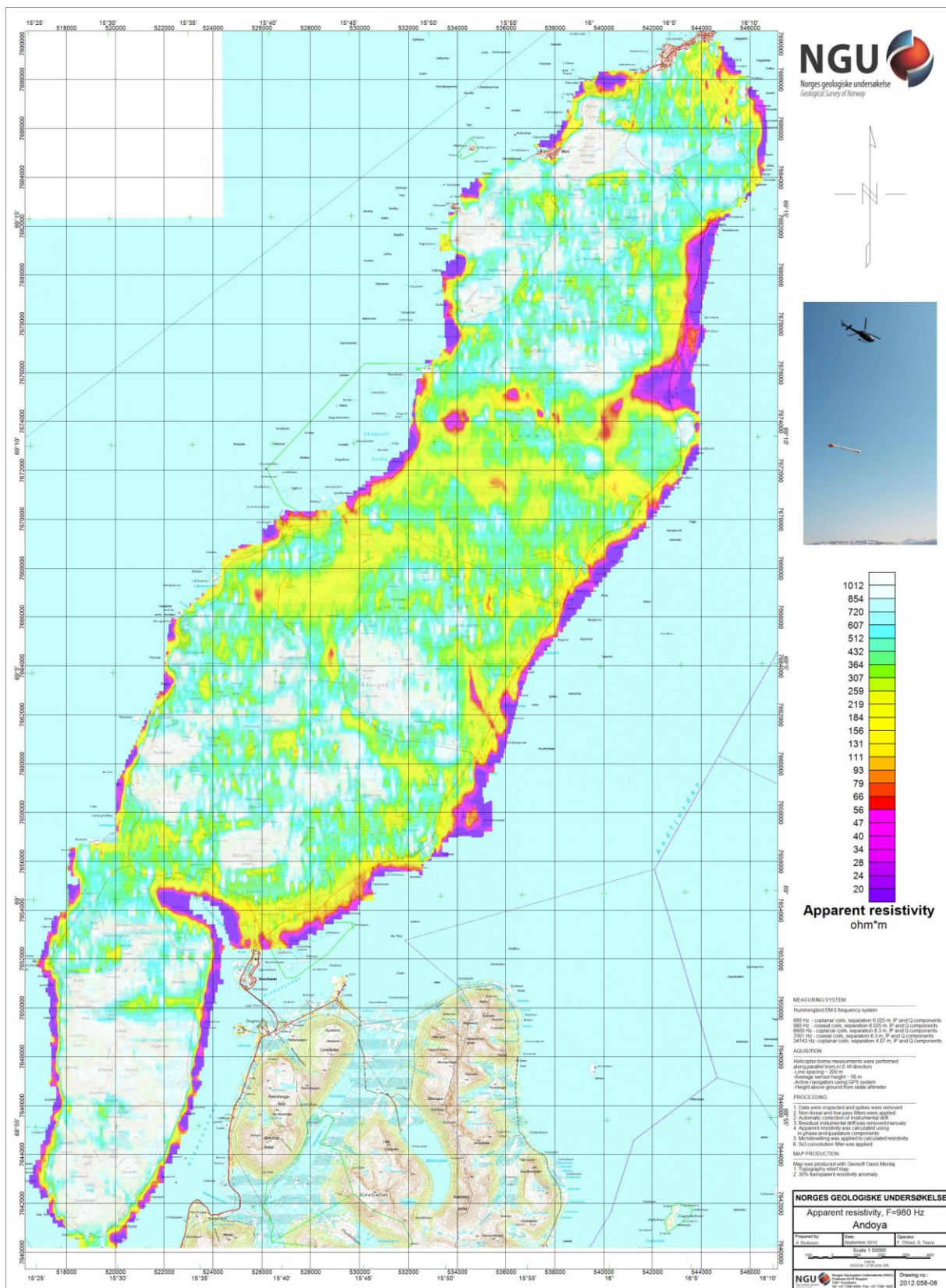


Figure 12: Apparent resistivity. Frequency 980 Hz, Coaxial coils



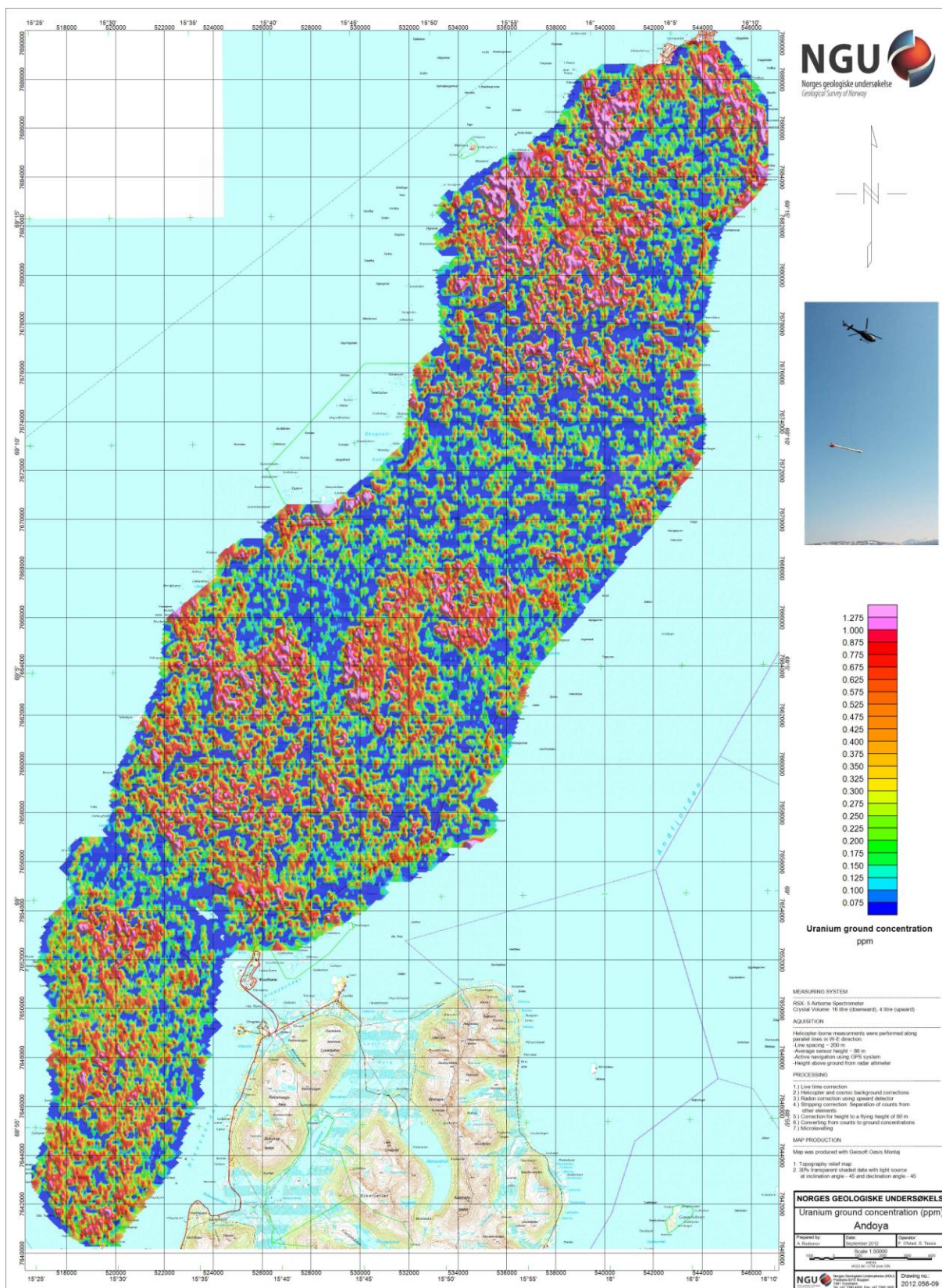


Figure 4 Uranium ground concentration



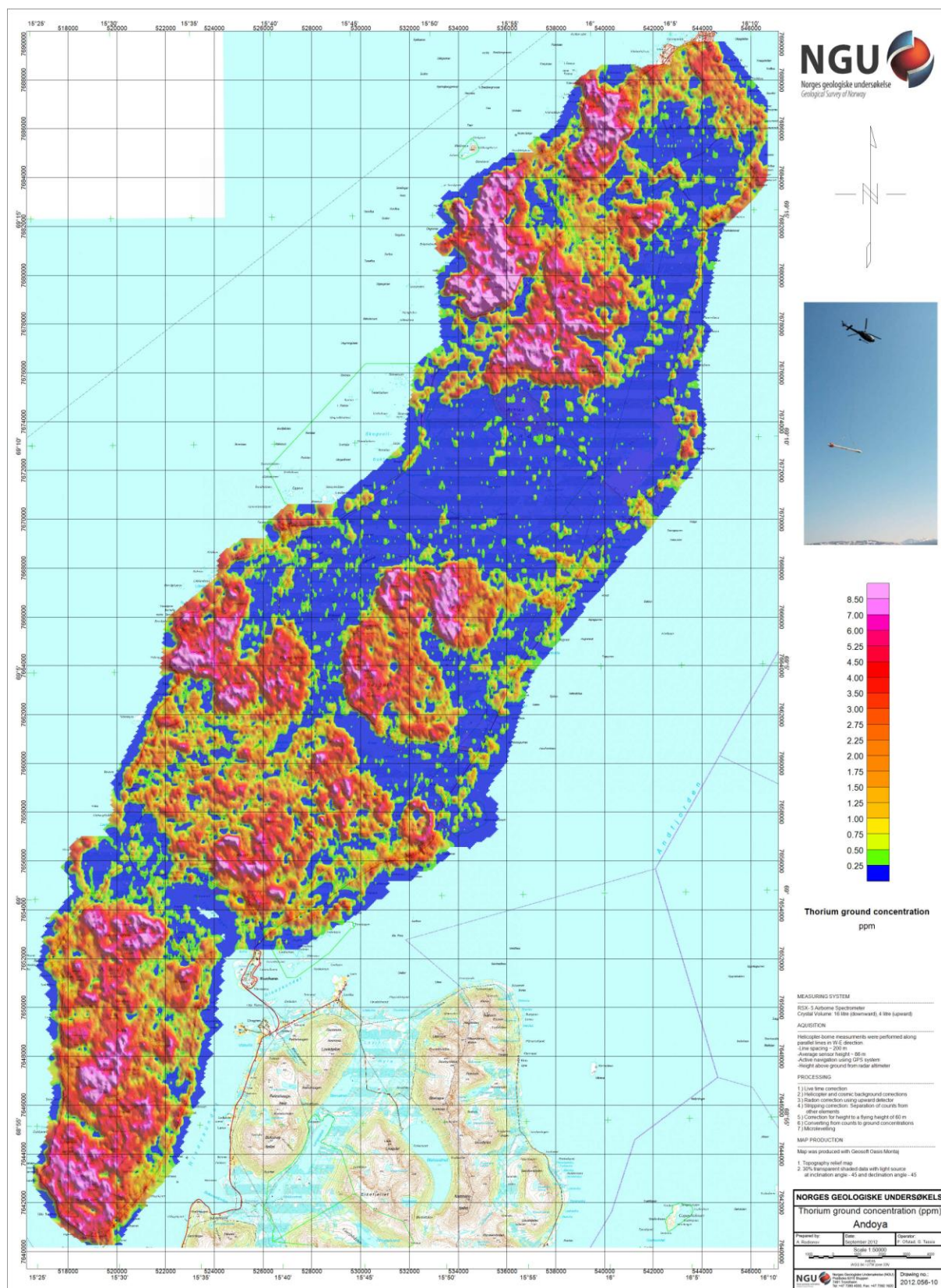


Figure 5 Thorium ground concentration



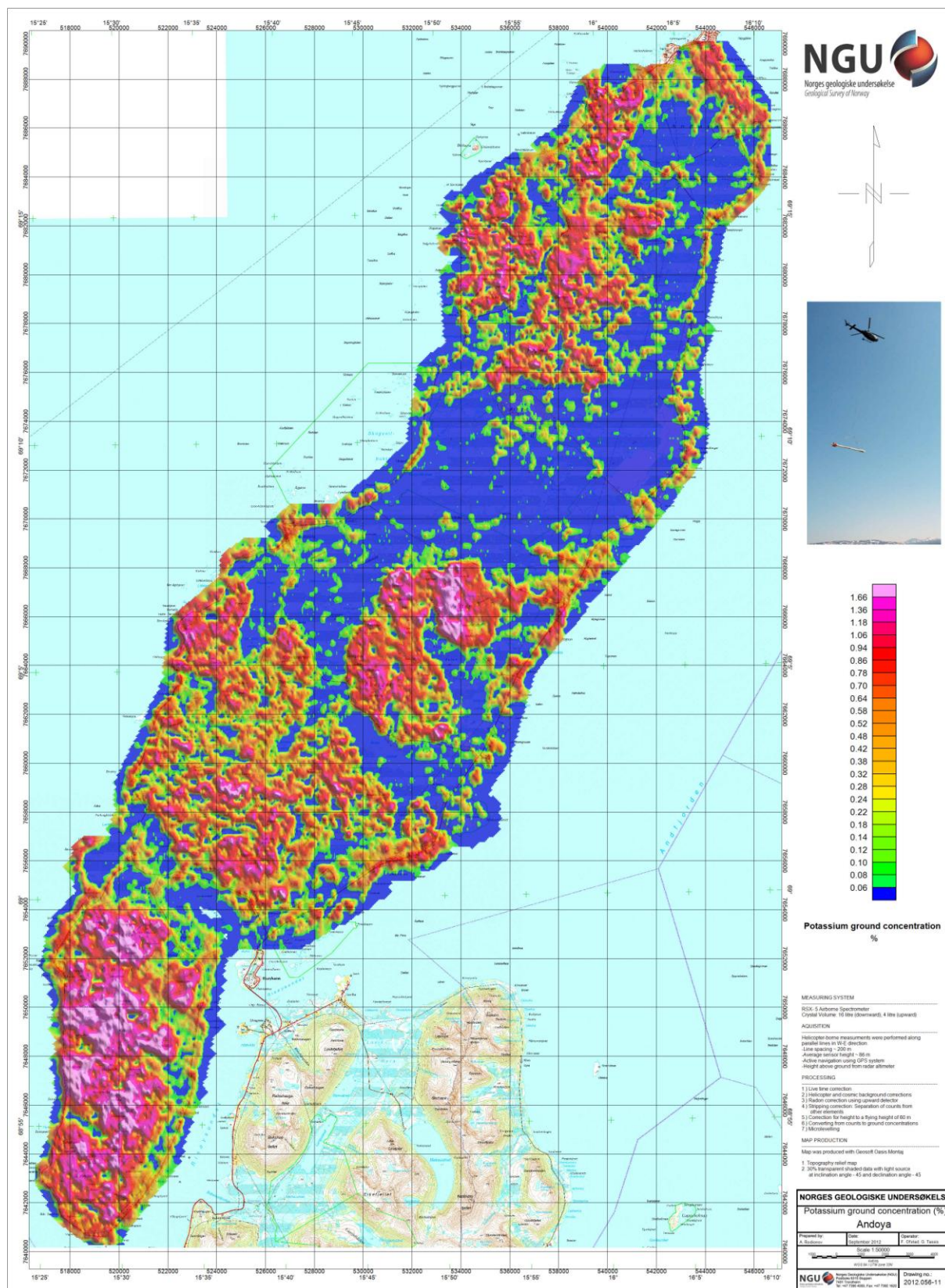


Figure 6 Potassium ground concentration



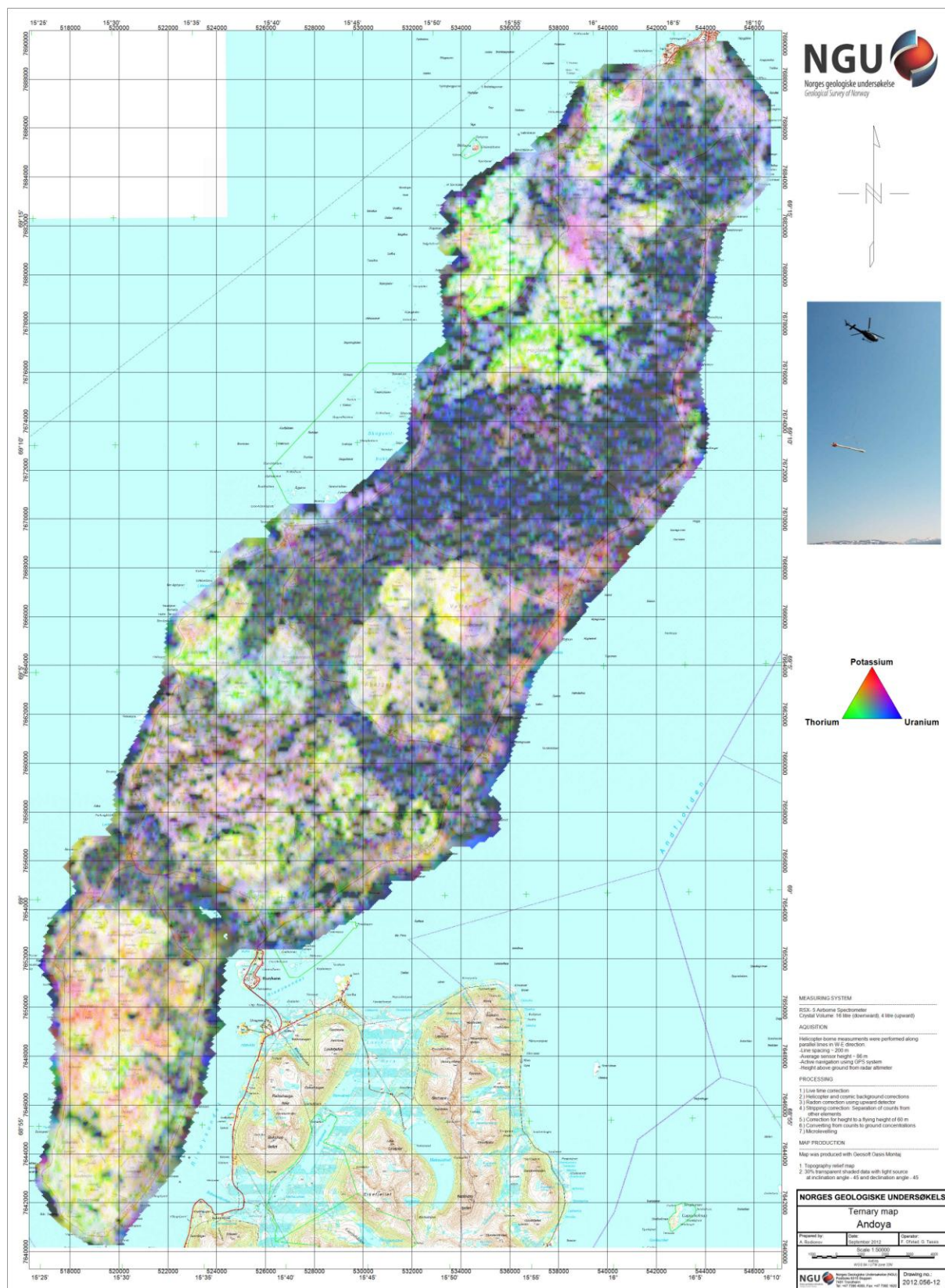


Figure 7 Radiometric ternary map

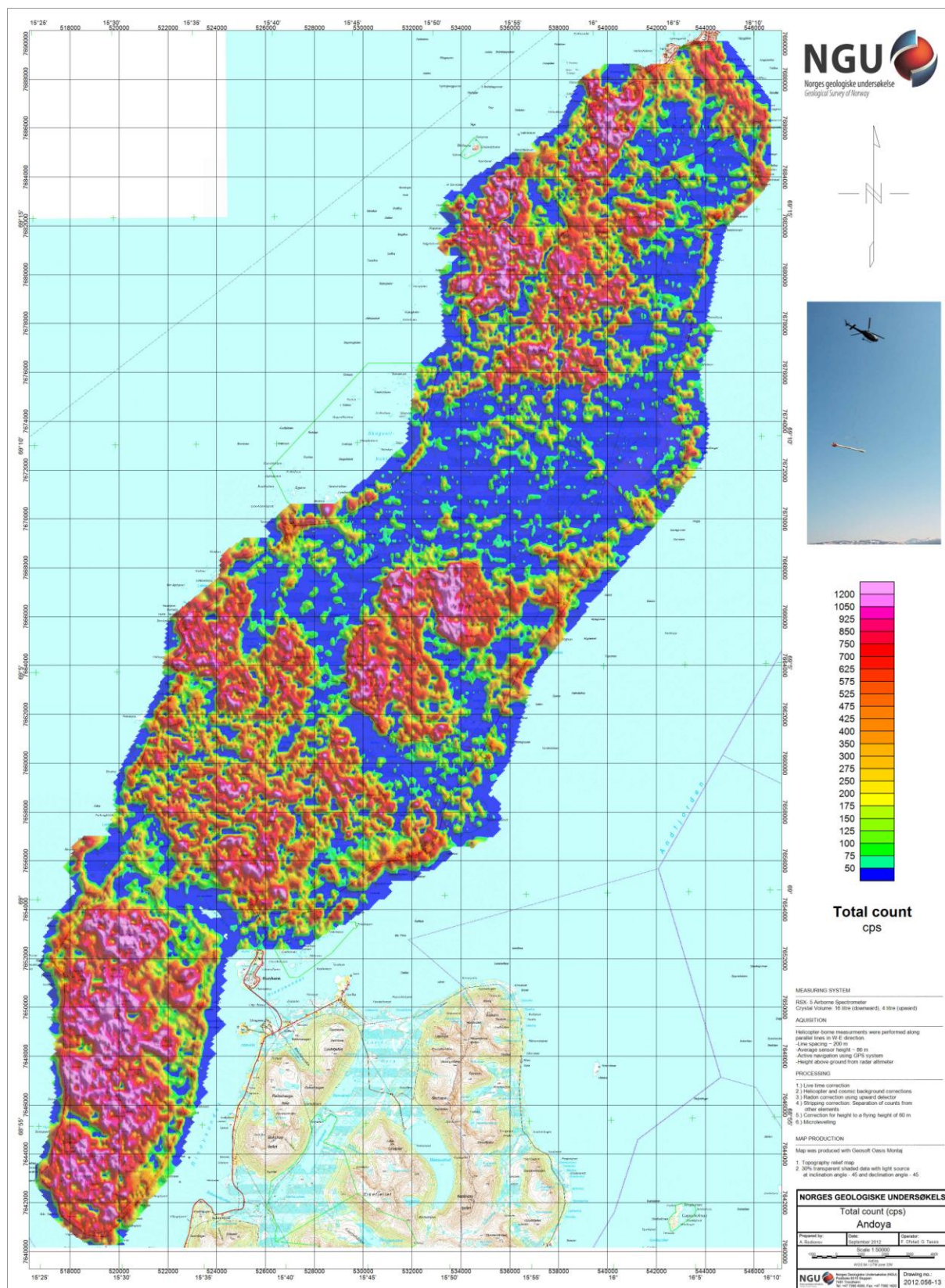


Figure 8 Radiometric total count.